

COCHLEAR EVANESCENT LIQUID SOUND-PRESSURE WAVES DURING SPONTANEOUS OTO-ACOUSTIC EMISSIONS

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1. INTRODUCTION

In the diagram on the left in Fig. 1, the streamlines of an evanescent (standing) liquid sound-pressure wave generated by a miniaturized and idealized underwater tuning-fork prong are shown [Frosch (2010a, 2010b)]. The prong is assumed to oscillate in the z_r -direction. Liquid particles having a no-wave location on one of these streamlines stay on that line during their oscillation. In the diagram on the right in Fig. 1, the corresponding lines of constant liquid sound-pressure amplitude are displayed; see Section 2.1.

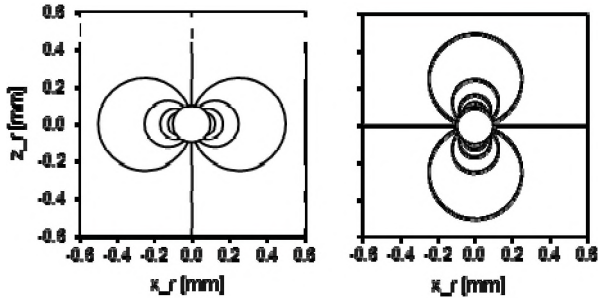


Figure 1. Underwater mini-tuning-fork prong oscillating in the z_r -direction. Left: streamlines. Right: lines of constant liquid sound-pressure amplitude.

In this study it is assumed that spontaneous oto-acoustic emissions (SOAEs) from the human inner ear [e.g., Frosch (2010a)] are generated, in a feedback process, by outer-hair-cell-driven localized oscillations of the basilar membrane (BM), and it is shown that a corresponding liquid motion above and below the BM of an idealized cochlear box model [cubic channel, x -independent properties] can be found by a superposition of three standing waves similar to that shown in Fig. 1, generated by a prong centred at $x_r = 0$ and by two prongs at $x_r = \pm a$, where typically $a = 0.01$ mm. It is assumed that at time $t = T/4$ (where $T =$ oscillation period) the central prong is at $z_r = +2\delta$ and the two lateral prongs are at $z_r = -\delta$; typically, $\delta = 0.1$ μm .

2. METHODS AND RESULTS

The liquid-particle oscillation amplitudes are small compared to the half-pressure distance of ~ 0.1 mm visible in Fig. 1. In the corresponding small-displacement approximation [see e.g. Frosch (2010a)] the sound-pressure p and the liquid-particle velocity v in a liquid of density ρ and of negligible compressibility and viscosity obey Newton's second law in the form

$$\rho \cdot (\partial \vec{v} / \partial t) = -\vec{\nabla} p, \quad (1)$$

and, in the present two-dimensional case, the Laplace equation,

$$\partial^2 p / \partial x^2 + \partial^2 p / \partial y^2 = 0. \quad (2)$$

A possible (standing-wave) solution for p is:

$$p(x, y, t) = a_p(x, y) \cdot \sin(\omega \cdot t), \quad (3)$$

where the angular frequency $\omega = 2\pi \cdot f$ is assumed to be constant. The real function $a_p(x, y)$ in Eq. (3) must fulfil the Laplace equation (2).

2.1. Oscillation of a “miniprongs” according to Fig. 1

As explained e.g. in Frosch (2010b), the real and imaginary parts of the function $F(n_c) = n_c^{-1}$ (where $n_c = x_r + i \cdot z_r$) yield the circular streamlines and lines of constant sound-pressure amplitude shown in Fig. 1. Streamlines:

$$r = R \cdot (N/n) \cdot \cos(\varphi); \quad (4)$$

$n = 0, \pm 1, \pm 2, \dots, \pm N$ is the running number of the streamlines; in Fig. 1 $N = 5$ was chosen; $R = 0.1$ mm is the prong radius; r and φ are plane polar coordinates:

$$r = \sqrt{x_r^2 + z_r^2}; \quad \tan(\varphi) = z_r / x_r. \quad (5)$$

Lines of constant sound-pressure amplitude:

$$r = R \cdot (a_{p0} / a_p) \cdot \sin(\varphi). \quad (6)$$

In Eq. (6), a_{p0} is a pressure constant, and a_p is defined by Eq. (3). The lines of constant liquid sound-pressure amplitude in Fig. 1 are for $a_p / a_{p0} = 0.0, \pm 0.2, \pm 0.4, \dots, \pm 1.0$.

2.2. Localized oscillation of the basilar membrane

The superposition described in Section 1 yields the following liquid sound-pressure amplitude [Frosch (2011)]:

$$\frac{a_p}{a_{p0}} = \frac{-R \cdot z_r}{x_r^2 + z_r^2} + \frac{0.5R \cdot z_r}{(x_r - a)^2 + z_r^2} + \frac{0.5R \cdot z_r}{(x_r + a)^2 + z_r^2}; \quad (7)$$

The corresponding streamlines are defined as follows:

$$\frac{q \cdot n}{N} = \frac{R \cdot x_r}{x_r^2 + z_r^2} - \frac{0.5R \cdot (x_r - a)}{(x_r - a)^2 + z_r^2} - \frac{0.5R \cdot (x_r + a)}{(x_r + a)^2 + z_r^2}; \quad (8)$$

the number q in Eq. (8) is the maximum of the expression on the right-hand side for $z_r = R$; for $R = 0.1$ mm and $a = 0.01$ mm one finds $q = 0.007224$; that maximum is located at $x_r = 41.7 \mu\text{m}$; see Fig. 3.

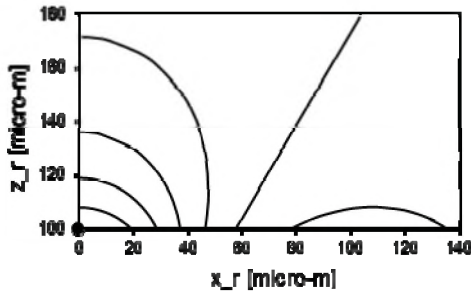


Figure 2. Constant-pressure lines, $a_p/a_{pmin} = 0.8, 0.6, 0.4, 0.2, 0.0, -0.2$, according to Eq. (7); a_{pmin} is the value of a_p at $x_r = 0$, $z_r = R = 0.1$ mm; the BM is at $z_r = R$.

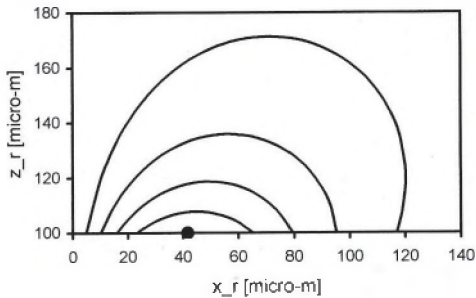


Figure 3. Streamlines according to Eq. (8), for $N = 5$.

The BM is assumed to have a negligible thickness and to be located at $z_r = R = 0.1$ mm. In the case of both Fig. 2 and Fig. 3, the patterns at $z_r < R$ (below the BM) and at $x_r < 0$ are mirror images of those shown.

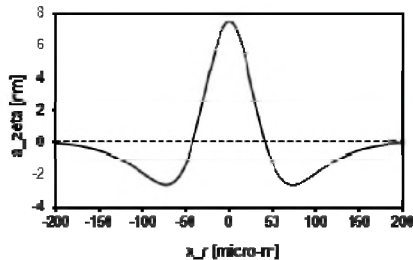


Figure 4. Shape of the basilar membrane at time $t = T/4$, according to Eqs. (1,3,7); $z_r = R = 100$ μ m; $a_{p0} = 1$ Pa; oscillation frequency $f = 1$ kHz; liquid density 1 g/cm³.

The amplitudes of the z -components $\zeta = a_z \cdot \sin(\omega t)$ of the displacements of the liquid particles in Figs. 2 and 3 from their no-wave locations x_r, z_r , according to Eqs. (1), (3), and (7), are given by Eq. (25) of Frosch (2011). The corresponding shape of the BM at time $t = T/4$ is shown in Fig. 4.

3. DISCUSSION AND CONCLUSIONS

The evanescent (standing) liquid sound-pressure wave described in Section 2.2 fulfils the Laplace equation. It is however incompatible with Newton's second law (force = mass \times acceleration) applied to the friction-less passive basilar-membrane (BM) elements of a cochlear box model [Frosch (2010a)] with x -independent BM stiffness S and

BM surface mass density M , and with negligible direct mechanical coupling of the BM elements. That disagreement can be corrected by introduction of a periodic force exerted on the BM by active outer hair cells (OHCs). In the present frictionless case, the OHC force must be proportional to $\sin(\omega t)$. In Fig. 5, the amplitude of the required force on a BM element of $5 \times 300 \mu\text{m}^2$, centred at x_r , is shown versus x_r for three different values of the assumed BM stiffness.

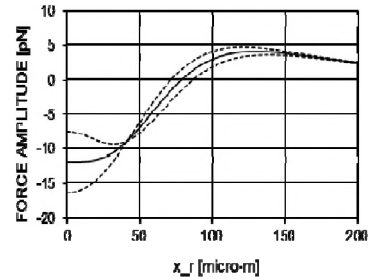


Figure 5. Active-outer-hair-cell force amplitude required by Newton's law (see text). Curves starting at $-16.4, -12.0$, and -7.6 pN are for $S/S_{res} = 1.3, 1.4$, and 1.5 .

The quantity S_{res} in the caption of Fig. 5 is the without-liquid BM resonance stiffness, $S_{res} = \omega^2 \cdot M$; e.g., if $S = 1.4 S_{res}$ (solid curve in Fig. 5), then for the parameters in the caption of Fig. 4 and for $M = 0.1$ kg/m², $t = T/4$, $x_r = 0$, the forces due to the BM stiffness, the liquid-pressure difference across the BM, and the active OHCs amount to $-62.0, +29.7$, and -12.0 pN. The resultant force, -44.3 pN, agrees with the downwards acceleration of the considered BM element. If both the liquid and the OHC force were removed, then the BM free-oscillation frequency in that box model with stiffness $S = 1.4 S_{res}$ would be $\sqrt{1.4} \cdot 1$ kHz = 1.18 kHz, higher than 1 kHz by about 0.24 octave.

In the real cochlea, "slow" travelling surface waves of given frequency [Frosch (2010a)] are impossible at the without-liquid BM resonance place for that frequency, but are possible at the corresponding with-liquid resonance place, which is more basal by typically 0.24 octave distance, i.e., by about 1.1 mm. From that place, the with-liquid BM oscillations conjectured to occur during spontaneous oto-acoustic emissions could be efficiently carried, by such slow cochlear travelling waves, to the cochlear base (oval window, stapes) and then propagate to the ear canal.

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