ACTIVE CONTROL OF PLATE VOLUME DISPLACEMENT: SIMULATION AND EXPERIMENTAL RESULTS

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1. INTRODUCTION

The two main strategies for actively controlling sound fields are the Active Noise Control (ANC) and the Active Structural Acoustic Control (ASAC), first proposed by [Fuller 1990]. The ANC approach is based on controlling the acoustic field itself by using loudspeakers as secondary sources, while the ASAC approach directly modifies the response of the radiating structure by using structural transducers as secondary sources. In general, the ASAC approach has been proved to require a smaller number of secondary sources for a global control of the acoustic field. Recently, piezoceramic actuators embedded in or bonded to the structure have been successfully used as structural secondary sources for active noise applications, see [Fuller *et al.* 1989], [Clark *et al.* 1992] and [Crawley *et al.* 1987]. These distributed actuators overcome many of the disadvantages of shakers.

In ASAC, the other component of prime importance is the error sensor, which defines the type of information to be minimized by the controller. Polyvinylidene fluoride (PVDF) materials have been suggested as error sensors in the active control of structural vibration [Lee *et al.* 1990], [Gu *et al.* 1992], and more recently in the active control of sound radiation [Clark *et al.* 1992a, 1993], [Guigou *et al.* 1994] and [Snyder *et al.* 1993], as an alternative to discrete microphones located in the acoustic field. [Guigou *et al.* 1994] developped a volume displacement sensor for beam using a single shaped PVDF strip. With this sensor, they have successfully implemented an active control of volume displacement for flexural beams and observed significant attenuation of the radiated sound field when active control was implemented. A similar approach was used by [Charette *et al.* 1995] to developed volume displacement sensor for 2D structure, i.e. rectangular plates. This plate volume displacement sensor is made of several shaped strips of PVDF film. This paper presents experimental results of an active control of volume displacement sensor is made of several shaped strips of PVDF volume displacement sensor as the error sensor.

2. ACTIVE CONTROL SIMULATION OF A PLATE VOLUME DISPLACEMENT

Active control simulation, for the clamped plate and actuators described in Tables 1 and 2, is performed to verify the efficiency of the proposed strategy (i.e. the minimization of the volume displacement) in reducing the sound radiation. To this end, the far-field radiated power and radiation efficiency are shown before and after control in Figure 1.

TABLE 1: Clamped plate characteristics				
Length	50.0 cm			
Width	39.8 cm			
Thickness	3.15 mm			
Young mod. (E)	6.5×10 ¹⁰ Pa			
Density (ρ)	2800 Kg/m ³			

TABLE 1: Clamped plate characteristics

It can be observed that below 220Hz, the radiation efficiency before control follows that of a monopole (about 6dB/oct.). Under control, in that frequency region, the radiation efficiency is changed to that of a dipole (about 12dB/oct.). The control of the plate volume displacement gives the largest sound power reduction in the frequency range where the radiation efficiency is reduced, since it decreases the plate capacity to induce sound in the acoustic medium.

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	Primary	Secondary
Length	3.81 cm	3.81 cm
Width	3.18 cm	3.18 cm
Thickness	0.19 mm	0.19 mm
Pos. along the x axis	16.0 cm	19.0 cm
Pos. along y axis	30.0 cm	15.0 cm
Young mod. (E)	6.3×10 ¹⁰ Pa	6.3×10 ¹⁰ Pa
Density (ρ)	7750 Kg/m ³	7750 Kg/m ³



Figure 1: Theoretical simulation of the active control of volume displacement.

Over 220Hz, the radiation efficiency is approximately the same before and after control. In this frequency range, the control mechanism becomes mostly an attenuation of the plate vibration. The control efficiency near a mode depends mainly on the volume displacement of that mode. The (3,3) mode (413Hz) is thus controlled, while the (2,1) (243Hz), the (1,2) (319Hz) and the (2,2) (415Hz) which have low volume displacement are practically not controlled.

It can be noted, that a peak appears at 460Hz after control. This is caused by the control actuator which as a low authority near this frequency. Due to his dimensions and position, near 460Hz the control actuator as difficulty to generate volume displacement. This implies a high voltage is needed to control and associated with this high voltage is a global increase in the vibration level which in turn yields the regeneration of radiated power. An optimization of the control actuator characteristics should allow to prevent such regeneration of the radiated power.

3. EXPERIMENTAL RESULTS

An experimental implementation using the plate of the previous section was done. Eight different frequencies were actively controlled using a LMS feedforward algorithm. Due to lack of space, only the results for the mode (1,1) at 140Hz are presented.





Figure 2(a) and 2(b) shows the plate transversal displacement before and after control respectively. Those two plot demonstrate that the plate displacement go from a monopole type radiator to a

dipole one. This confirm that the PVDF volume displacement sensor works properly. Figure 2(c) presents pressure level measurements made in the plane x=0. This plot shows a significant attenuation (between 40 and 50dB) in the pressure level at this frequency. Such attenuation is possible because at this frequency the control of the volume displacement minimizes the radiation efficiency and the vibration level simultaneously.

CONCLUSIONS

At low frequencies, passive control methods are generally inefficient for reducing the sound power radiated by a structure. However, the results presented in this paper clearly shows that the active control of volume displacement provides significant attenuation of sound radiation at those frequencies.

For the clamped plate considered here, the results indicates that below 220Hz the active control of volume displacement reduces the plate radiation efficiency and vibration level simultaneously. While over 220Hz, the control of volume displacement corresponds mainly to a reduction of the vibration level.

Using extended transducers, such as PVDF film, allows to have a single error channel to reduce the sound power radiated. This greatly simplifies the implementation of an active control system in the real world.

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REFERENCES

Charette F., Guigou C. and Berry A. "Development of volume velocity sensors for plates using PVDF film", *Proceedings of ACTIVE95 The 1995 International Symposium on Active Control of Sound and Vibration*, pages 241-252 (1995).

Clark R.L. and Fuller C.R. "Experiments on active control of structurally radiated sound using multiple piezoelectric actuators", J. Acoust. Soc. Am. 91(6), pages 3313-3320 (1992).

Clark R.L. and Fuller C.R. "Modal sensing of efficient acoustic radiators with PVDF distributed sensors in active structural acoustic approaches", J. Acoust. Soc. Am. 91(6), pages 3321-3329 (1992a).

Clark R.L., Burdisso R.A. and Fuller C.R. "Design approaches for shaping polyvinylidene fluoride sensors in active structural acoustic control (ASAC)", *Journal of Intelligent Material Systems* and Structures, 4, pages 354-365 (1993).

Crawley E.F. and de Luis J. "Use of piezoelectric actuators as elements of intelligent structures", *AIAA Journal*, **25**(10), pages 1373-1385 (1987).

Fuller C.R., Hansen C.H. and Snyder S.D. "Active control of structurally radiated noise using piezoceramic actuator", *Proceedings of Inter-Noise 89*, pages 509-511 (1989).

Fuller C.R. "Active control of sound transmission/radiation from elastic plates by vibrational inputs: I. Analysis", *Journal of Sound and Vibration*, **136**(1), pages 1-15 (1990).

Gu Yi, Clark R.L., Fuller C.R. and Zander A.C. "Experiments on active control of plate vibration using piezoelectric actuators and polyvinylidene (PVDF) modal sensors", submitted to the *Journal of Sound and Vibration*, (1992).

Guigou C., Charette F. and Berry A. "Active control of sound by minimization of volume velocity on finite beam", *Proceedings of the Third International Congress on Air- and Structure-borne Sound and vibration*, pages 1507-1514 (1994).

Lee C.K., Moon F.C., "Modal sensors / actuators", *Transactions of the ASME*, **57**, pages 434-441 (1990).

Snyder S.D., Hansen C.H. and Tanaka N. "Shaped vibration sensors for feedforward control of structural radiation", *Proceedings of the Second Conference on the Recent Advances in Active Control of Sound and vibration*, pages 177-188 (1993).